### 3.5A,30V Step Down Converter with Supporting Fast Charging Protocol

# **Description**

NDP133A1KC is a high efficiency, monolithic synchronous step-down DC/DC converter integrated with multiple USB Dedicated Charging Protocol. The step-down converter can deliver up to 3.5A continuous load with excellent line and load regulation over input voltage range of 8.5V to 30V.

The integrated USB Dedicated Charging protocol complies with the most popular fast charging protocol as QC2.0. /3.0, SCP, FCP, and AFC etc. It also supports Apple iPhone, BC1.2 or YD/T 1591 compliant devices. An auto-detect feature automatically identifies the handheld devices attached to the USB port, and automatically adjusts output voltage.





### **Features**

- Wide VIN Range: 8.5V to 30V
- 3.5A Continuous Output Current
- Up to 95% Efficiency
- CC/CV Mode Control
- 100% Max Duty Cycle •
- Default 5.1V fixed Output Voltage
- +/-2% Output Voltage Accuracy
- Internal loop Compensation
- Integrated 45/21 mΩ High/Low Side RDS(ON) •
- Burst Mode Operation at Light Load

### **USB Dedicated Charging Protocol**

- Output voltage range: 3.6V~12V, adjust along ۲ with fast charge negotiation
- Support Qualcomm Quick Charge 2.0/3.0
- Support SCP/FCP /AFC
- Support USB DCP applying 2.7V on D+/ D-
- Meets BC1.2, YD/T 1591-2009
- QC 3.0 Certification: QC20230629328
- Available in SOP8 Package

## **Applications**

- Wall-Adapter, Smart phones
- Car Charger
- Tablets, Netbooks
- **Distributed Power Systems**



**Typical Application** 



Top Side Marking

# **Order Information**

Orderable	Package	Packing	MSL- Peak Temp	Eco	Marking
Device	Type	Qty/reel	-Floor Life	Std	Information
NDP133A1KC	SOP8	4000	MSL3-260°C-168hrs	RoHS & Green	Refer to below

### **Product Naming**



### Notes:

- (1) RoHS: Quoted from RoHS Detective (EU) 2015/863, Deep-Pool defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. Deep-Pool may reference these types of products as "Pb-Free".
- (2) **RoHS Exempt:** Deep-Pool defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.
- (3) **Green**: Deep-Pool defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JEDEC (**JS709C**) low halogen requirements of <=1000ppm threshold.

(4) **MSL**, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC (**J-STD-020F**) industry standard classifications, as well as the peak solder temperature of SMT and the floor life after unpacking, which customers should pay attention and strictly comply with the standard to use.

(5) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

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## **Pin Function and Definition**

Pin	Name	Definition
1	VOUT	Feedback Of Output Voltage
2	DP	Connect to D+ of USB Dataline
3	DM	Connect to D- of USB Dataline
4	VIN	Power Input Positive Pole
5,6	SW	Switching, Connected With a Inductor
7	NC	No Connection
8	GND	Ground



# Absolute Maximum Ratings (at T<sub>A</sub>= 25°C)

Characteristics	Symbol	Rating	Unit
VIN to GND		-0.3 to 33	V
SW to GND		-0.3 to VIN+0.3	V
DP、DM to GND		-0.3 to 25	V
VOUT to GND		-0.3 to 25	V
Operating Junction Temperature	T <sub>A</sub>	-40 to 150	°C
Storage Junction Temperature	Tstg	-65 to 150	°C
Thermal Resistance from Junction to case	$\theta_{JC}$	45	°C/W
Thermal Resistance from Junction to ambient	θ <sub>JA</sub>	90	°C/W

### Notes:

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

RECOMMENDED OPERATING RANGE						
ELECTRICAL PARAMETER	MINIMUM	TYPICAL	MAXIMUM	UNIT		
Input Voltage (V <sub>IN</sub> )	9.5		24	V		
Output Current (I <sub>OUT</sub> )			3.5	А		



# **Electrical Characteristics**

 $T_J = 25^{\circ}C$ ,  $V_{IN} = 12V$ , unless otherwise noted.

Characteristics	Symbol	Conditions	Min	Тур.	Max	Units
Step Down Converter						
Input Voltage	V <sub>IN</sub>		8.5	-	30	V
Input Over Voltage Protect	V <sub>OVP</sub>		-	32	-	V
Quiescent Current	I <sub>CCQ</sub>	no switch	-	0.3	-	mA
Standby Current	I <sub>SB</sub>	No Load	-	0.45	-	mA
VOUT Feedback Voltage	V <sub>OUT</sub>		5.0	5.1	5.2	V
Switching Frequency	Fsw		-	120	-	KHz
Minimum On-Time			-	300	-	nS
Current Limit	I <sub>LIM</sub>	Current limit	4.5		-	А
Output Voltage Short Protect	V <sub>OUT SCP</sub>		-	2.4	-	V
Hiccup Interval	Thiccup		-	330	-	mS
Soft Start Time	T <sub>SS</sub>		-	8	-	mS
PDSON Of Power MOS	R <sub>DSON_H</sub>	Temp=25°C	-	45	-	mΩ
KDSON OFFOWER MOS	R <sub>DSON_L</sub>	Temp=25°C	-	21	-	mΩ
Thermal Regulation	T <sub>TR</sub>		-	140	-	°C
Thermal Shutdown	T <sub>SD</sub>		-	160	-	°C
USB Dedicated Charging Port	1	1				I
Data Detect Voltage	VDAT(REF)		0.25	0.325	0.4	V
Output Voltage Selection	Vary and		1.8	2.0	2.2	V
Reference	▼ SEL_REF		1.0	2.0	2.2	v
D+ High Glitch Filter Time	T <sub>GLITCH(BC)</sub> -D+_H		800	1250	1500	mS
D- Low Glitch Filter Time	T <sub>GLITCH(BC)</sub> -DL			1		mS
Output Voltage Glitch Filter	T <sub>GLITCH</sub> (V)CHANG			40		mS
Time	Е			40		1115
D- Pull-Down Resistance	R <sub>D-(DWN)</sub>			20		KΩ
Continuous Mode Glitch Filter	T <sub>GLITCH</sub> -cont-ch		100		200	115
Time	ANGE		100		200	uS
D+ Leakage Resistance	R <sub>DAT-LKG</sub>		300	400	500	KΩ
Switch SW1 on-resistance	R <sub>DS_ON_N1</sub>				40	Ω
Up/Down Current Step	I <sub>UP</sub> / IDOWN			2		uA
DP Output Voltage	V <sub>DPX_2.7</sub>		2.6	2.7	2.8	V



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DM Output Voltage	V <sub>DMX_2.7</sub>	2.6	2.7	2.8	V
DP Output Impedance	R <sub>DPX</sub>	24	30	36	KΩ
DM Output Impedance	R <sub>DMX</sub>	24	30	36	KΩ



# **Typical Performance Characteristics**

 $(TJ = 25^{\circ}C, unless otherwise noted.)$ 











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CH1=Vin, CH2=Vout, CH3=SW, CH4=Isw,5mS/div



CH1=Vin, CH2=Vout, CH3=SW, CH4=Isw,10uS/div



CH1=Vin, CH2=Vout, CH3=SW, CH4=Isw ,100mS/div



CH1=Vin, CH2=Vout, CH3=SW, CH4=Isw, 5mS/div



CH1=Vin, CH2=Vout, CH3=SW, CH4=Isw, 10uS/div



CH1=Vin, CH2=Vout, CH3=SW, CH4=Isw ,100mS/div



# **Block Diagram**



# **Operational Description**

NDP133A1KC is a high efficiency, monolithic synchronous step-down DC/DC converter integrated with multiple USB Dedicated Charging Protocol. The step-down converter is Capable of delivering up to 3.5A continuous load with excellent line and load regulation over input voltage range of 8.5V to 30V.

The integrated USB Dedicated Charging protocol complies with the most popular fast charging protocol as QC2.0. /3.0, SCP,FCP, SCP and AFC etc. It also supports Apple iPhone, BC1.2 or YD/T 1591 compliant devices. An auto-detect

feature automatically identifies the handheld devices attached to the USB port, and automatically adjusts output voltage.

### **Main Control Loop**

During normal operation, the internal top power switch (P-channel MOSFET) is turned on at the beginning of each clock cycle, causing the inductor current to increase. The sensed inductor current is then delivered to the average current amplifier, whose output is compared with a saw-tooth ramp. When the voltage exceeds the vduty voltage, the PWM comparator trips and turns off the top power MOSFET. After the top power MOSFET turns off,



the synchronous power switch (N-channel MOSFET) turns on, causing the inductor current to decrease. The bottom switch stays on until the beginning of the next clock cycle, unless the reverse current limit is reached and the reverse current comparator trips. In closed-loop operation, the average current amplifier creates an average current loop that forces the average sensed current signal to be equal to the internal ITH voltage. Note that the DC gain and compensation of this average current loop is automatically adjusted to maintain an optimum current-loop response. The error amplifier adjusts the ITH voltage by comparing the divided-down output voltage with reference voltage. If the load current changes, the error amplifier adjusts the average inductor current as needed to keep the output voltage in regulation.

#### Low Current operation

The discontinuous-conduction modes (DCMs) are available to control the operation of the NDP133A1KC at low currents. Burst Mode operation automatically switch from continuous operation to the Burst Mode operation when the load current is low.

#### VIN Overvoltage Protections

In order to protect the internal power MOSFET devices against transient voltage spikes, the NDP133A1KC constantly monitors the VIN pin for an overvoltage condition. When VIN rises above 32V, the regulator suspends operation by shutting off both power MOSFETs. Once VIN drops below 30V, the regulator immediately resumes normal operation. The regulator executes its soft-start function when exiting an overvoltage condition.

### **Applications Information**

### Input Capacitor (CIN) Selection

The input capacitance CIN is needed to filter the

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square wave current at the drain of the top power MOSFET. To prevent large voltage transients from occurring, a low ESR input capacitor sized for the maximum RMS current should be used. The maximum RMS current is given by:

$$I_{RMS} \cong I_{OUT(MAX)} \frac{V_{OUT}}{V_{IN}} \sqrt{\frac{V_{IN}}{V_{OUT}}} - 1$$

This formula has a maximum at VIN = 2VOUT, where: IRMS  $\approx$  IOUT/2

This simple worst-case condition is commonly used for design because even significant deviations do not offer much relief. Note that ripple current ratings from capacitor manufacturers are often based on only 2000 hours of life which makes it advisable to further derate the capacitor, or choose a capacitor rated at a higher temperature than required. Several capacitors may also be paralleled to meet size or height requirements in the design. For low input voltage applications, sufficient bulk input capacitance is needed to minimize transient effects during output load changes.

### **Output Capacitor (COUT) Selection**

The selection of COUT is determined by the effective series resistance (ESR) that is required to minimize voltage ripple and load step transients as well as the amount of bulk capacitance that is necessary to ensure that the control loop is stable. Loop stability can be checked by viewing the load transient response. The output ripple,  $\triangle$  VOUT, is determined by:

$$\Delta V_{\text{OUT}} < \Delta I_{\text{L}} \left( \frac{1}{8 \bullet f \bullet C_{\text{OUT}}} + \text{ESR} \right)$$

The output ripple is highest at maximum input voltage since  $\triangle$  IL increases with input voltage. Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling requirements. Dry tantalum, special polymer, Rev1.2 Page #9-13

aluminum electrolytic, and ceramic capacitors are all available in surface mount packages. Special polymer capacitors are very low ESR but have lower capacitance density than other types. Tantalum capacitors have the highest capacitance density but it is important to only use types that have been surge tested for use in switching power supplies. Aluminum electrolytic capacitors have significantly higher ESR, but can be used

in cost-sensitive applications provided that consideration is given to ripple current ratings and long-term reliability. Ceramic capacitors have excellent low ESR characteristics and small footprints.

Inductor Selection

Given the desired input and output voltages, the

Once the value for L is known, the type of inductor must be selected. Actual core loss is independent of core size for a fixed inductor value, but is very dependent on the inductance selected. As the inductance or frequency increases, core losses Unfortunately, increased inductance decrease. requires more turns of wire and therefore copper losses will increase. Copper losses also increase as frequency increases Ferrite designs have very low core losses and are preferred at high switching frequencies, so design goals can concentrate on copper loss and preventing saturation. Ferrite core material saturates "hard", which means that inductance collapses abruptly when the peak design current is exceeded. This results in an abrupt increase in inductor ripple current and consequent output voltage ripple. Do not allow the core to saturate! Different core materials and shapes will change the size/current and price/current relationship of an inductor. Toroid or shielded pot cores in ferrite

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inductor value and operating frequency determine the ripple current:

$$\Delta I_{L} = \frac{V_{OUT}}{f \bullet L} \left( 1 - \frac{V_{OUT}}{V_{IN(MAX)}} \right)$$

Lower ripple current reduces power losses in the inductor, ESR losses in the output capacitors and output voltage ripple. Highest efficiency operation is obtained at low frequency with small ripple current. However, achieving this requires a large inductor. There is a trade-off between component size, efficiency and operating frequency. A reasonable starting point is to choose a ripple current that is about 40% of IOUT(MAX). To guarantee that ripple current does not exceed a specified maximum, the inductance should be chosen according to:

$$L = \frac{V_{OUT}}{f \bullet \Delta I_{L(MAX)}} \left( 1 - \frac{V_{OUT}}{V_{IN(MAX)}} \right)$$

or permalloy materials are small and don't radiate much energy, but generally cost more than powdered iron core inductors with similar characteristics. The choice of which style inductor to use mainly depends on the price versus size requirements and any radiated field/EMI requirements. New designs for surface mount inductors are available from Coilcraft, Toko, Vishay, NEC/Tokin, TDK and Würth Electronik.

#### **Efficiency Considerations**

The percent efficiency of a switching regulator is equal to the output power divided by the input power times 100%. It is often useful to analyze individual losses to determine what is limiting the efficiency and which change would produce the most improvement. Percent efficiency can be expressed as: % Efficiency = 100% - (Loss1 + Loss2 + ...)where Loss1, Loss2, etc. are the individual losses as a percentage of input power. Although all dissipative elements in the circuit produce losses, three main

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sources usually account for most of the losses in NDP133A1KC circuits: 1) I2R losses, 2) switching and biasing losses, 3) other losses.

### **Thermal Conditions**

In most applications, the NDP133A1KC does not dissipate much heat due to its high efficiency and low thermal resistance. However, in applications where the NDP133A1KC is running at high ambient temperature, high VIN, and maximum output current load, the heat dissipated may exceed the maximum junction temperature of the part. If the junction temperature reaches approximately 160°C, both power switches will be turned off until the temperature drops about 10°C cooler To avoid the NDP133A1 from exceeding the maximum junction temperature, the user will need to do some thermal analysis. The goal of the thermal analysis is to determine whether the power dissipated exceeds the maximum junction temperature of the part. If the application calls for a higher ambient temperature and/or higher switching frequency, care should be taken to reduce the temperature rise of the part by using a heat sink or forced air flow.

# **Typical Applications**





# Package Outline Drawing







Symbol	Dimensions	In Millimeters	Dimensions In Inches		
	Min	Max	Min	Max	
А	1.350	1.750	0.053	0.069	
A1	0.050	0.250	0.002	0.010	
A2	1.250	1.650	0.049	0.065	
b	0.310	0.510	0.012	0.020	
С	0.170	0.250	0.006	0.010	
D	4.700	5.150	0.185	0.203	
E	3.800	4.000	0.15	0.157	
E1	5.800	6.200	0.228	0.244	
e	1.270 (BSC)		0.05 (BSC)		
L	0.400	1.270	0.016	0.050	
θ	0°	8°	0°	8°	

### Notes

- 1. Use millimeters as the primary measurement
- 2. Dimensioning and tolerances conform to ASME Y14.5M. 1994
- 3. These dimensions do not include mold flash or protrusions.
- 4. Mold flash or protrusions shall not exceed 0.15mm



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