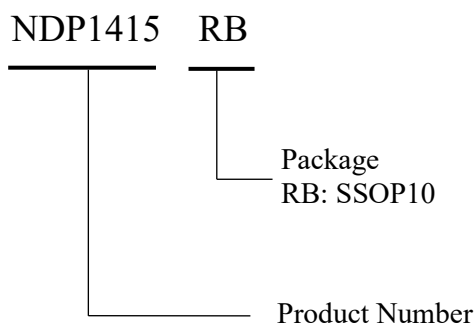


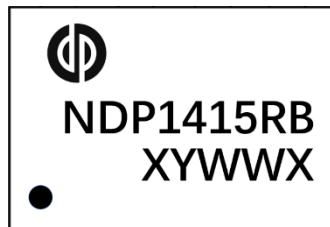
Order Information

| Orderable Device | Package Type | Packing Qty/reel | MSL- Peak Temp -Floor Life | Eco Std | Marking Information |
|------------------|--------------|------------------|----------------------------|--------------|---------------------|
| NDP1415RB | SSOP10 | 4000 | MSL3-260°C-168hrs | RoHS & Green | Refer to below |

Product Naming



Top Side Marking



X/X: Internal ID Code
Y: Year (3=2023,4=2024...)
WW: Weekly (01-53)

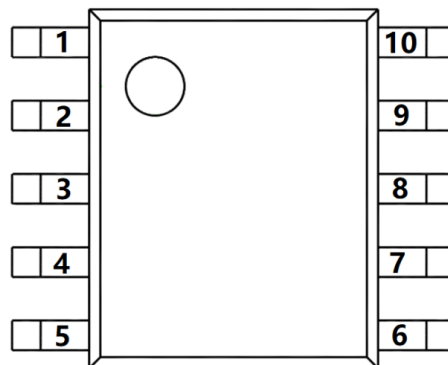
Notes:

- (1) **RoHS:** Quoted from **RoHS Directive (EU) 2015/863**, Deep-Pool defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. Deep-Pool may reference these types of products as "**Pb-Free**".
- (2) **RoHS Exempt:** Deep-Pool defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.
- (3) **Green:** Deep-Pool defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JEDEC (**JS709C**) low halogen requirements of ≤ 1000 ppm threshold.
- (4) **MSL, Peak Temp. -** The Moisture Sensitivity Level rating according to the JEDEC (**J-STD-020F**) industry standard classifications, as well as the peak solder temperature of SMT and the floor life after unpacking, which customers should pay attention and strictly comply with the standard to use.
- (5) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

The information provided on this page represents **Deep-Pool's** knowledge and belief as of the date that it is provided. **Deep-Pool** bases its knowledge and belief on information provided by third parties and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. **Deep-Pool** has taken and continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. **Deep-Pool** and **Deep-Pool** suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

Pin Function and Definition

| PIN | NAME | Description |
|-----|------|--|
| 1 | VIN | Power Input |
| 2 | HG | High Side MOSFET Driver |
| 3 | SW | Switching Pin, Connected with an Inductor |
| 4 | BST | Boot Strap |
| 5 | LG | Low Side MOSFET Driver |
| 6 | GND | Ground |
| 7 | FB | Feedback Of Output Voltage |
| 8 | CSP | Positive Pole of Current Sense |
| 9 | CSN | Negative Pole of Current Sense |
| 10 | FS | Connect a Resistor to GND for Frequency Config |



Absolute Maximum Ratings (at TA = 25°C)

| Characteristics | Symbol | Rating | Unit |
|---|---------------|-----------------|------|
| VIN to GND | | -0.3 to 44 | V |
| SW to GND | | -0.3 to VIN+0.3 | V |
| HG, BST to GND | | -0.3 to VIN+7.5 | V |
| LG to GND | | -0.3 to 7.5 | V |
| FB, FS to GND | | -0.3 to 6 | V |
| CSP, CSN to GND | | -0.3 to 25 | V |
| Operating Junction Temperature | TA | -40 to 150 | °C |
| Storage Junction Temperature | Tstg | -65 to 150 | °C |
| Thermal Resistance from Junction to case | θ_{JC} | 45 | °C/W |
| Thermal Resistance from Junction to ambient | θ_{JA} | 70 | °C/W |

Notes:

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

Recommended Operating Range

| ELECTRICAL PARAMETER | MINIMUM | TYPICAL | MAXIMUM | UNIT |
|-----------------------|---------|---------|---------|------|
| Input Voltage (VIN) | 8 | | 36 | V |
| Output Voltage (VOUT) | 3.3 | | 20 | V |
| Output Current (IOUT) | | 15 | | A |

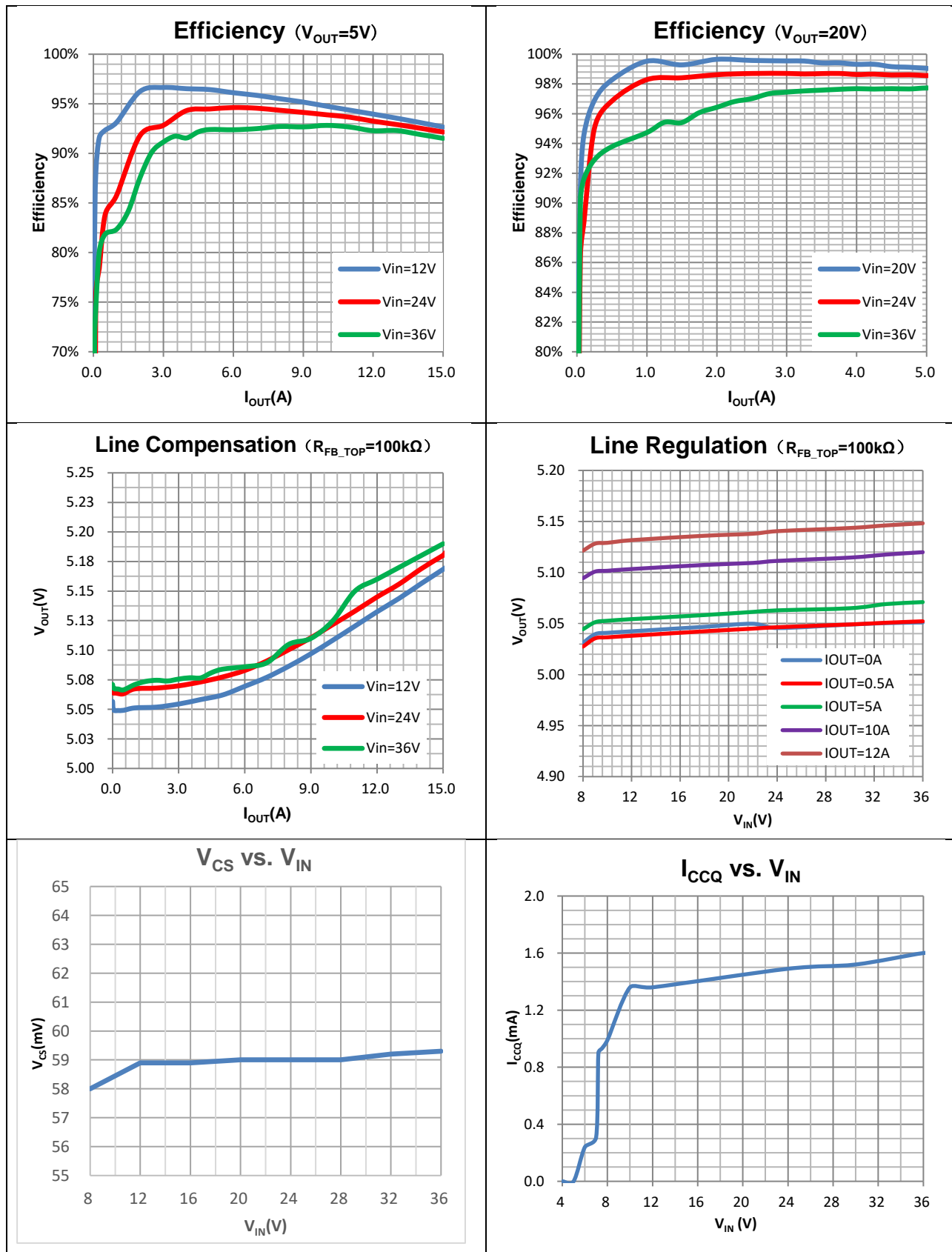
Electrical Characteristics

$T_J = 25^{\circ}\text{C}$, $V_{IN} = 12\text{V}$, unless otherwise noted.

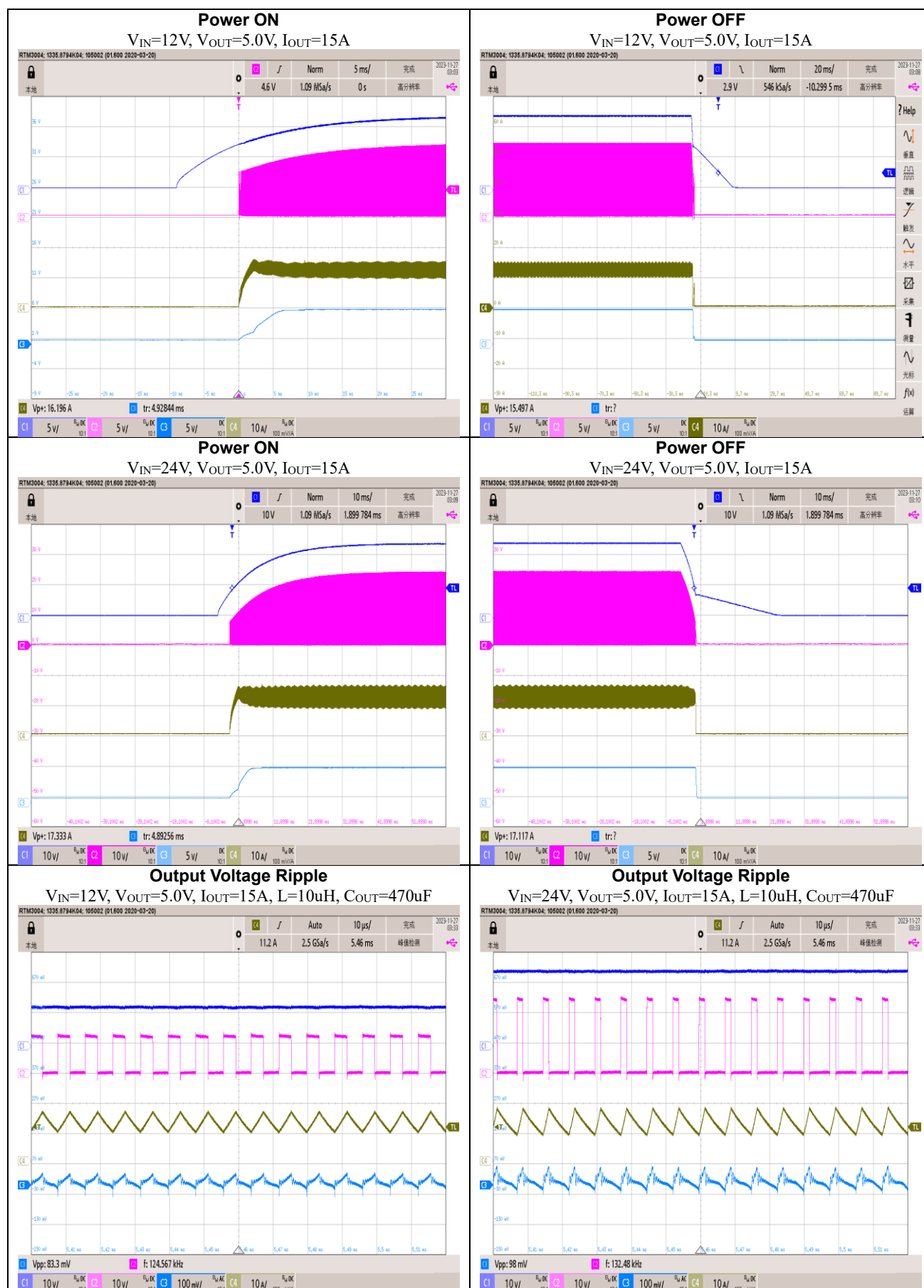
| Characteristics | Symbol | Conditions | Min | Typ | Max | Units |
|---|-----------------|-----------------------|------|------|------|--------------------|
| Input Voltage | V_{IN} | | 7.5 | - | 37 | V |
| UVLO OFF Voltage | V_{UVLO_OFF} | VIN Rising | | 7.2 | | V |
| UVLO ON Voltage | V_{UVLO_ON} | VIN Falling | | 6.7 | | V |
| VIN Overvoltage Protections | V_{OVP} | | 37 | 38 | 39 | V |
| Quiescent Current | I_{CCQ} | VFB = 1.2V, No Switch | - | 1300 | - | μA |
| Standby Current | I_{SB} | No Load | - | 1.7 | 2.2 | mA |
| FB Reference Voltage | V_{FB} | | 0.98 | 1 | 1.02 | V |
| Current Sense AMP | V_{CS} | CSP-CSN | 56 | 60 | 64 | mV |
| Switching Frequency | F_{SW} | FS Floating | | 130 | | kHz |
| | | connect 150K Resister | | 300 | | kHz |
| Maximum Duty Cycle | | | | 95 | - | % |
| Minimum On-Time | | | - | 250 | - | ns |
| VOUT short Protections | V_{SCP} | | | 3.0 | | V |
| Hiccup Interval | T_{HICCUP} | | | 500 | | mS |
| Soft Start Time | T_{SS} | | | 2 | | mS |
| Thermal Shutdown Temperature | T_{SD} | | - | 165 | - | $^{\circ}\text{C}$ |
| Thermal Shutdown Hysteresis Temperature | T_{SH} | | - | 30 | - | $^{\circ}\text{C}$ |

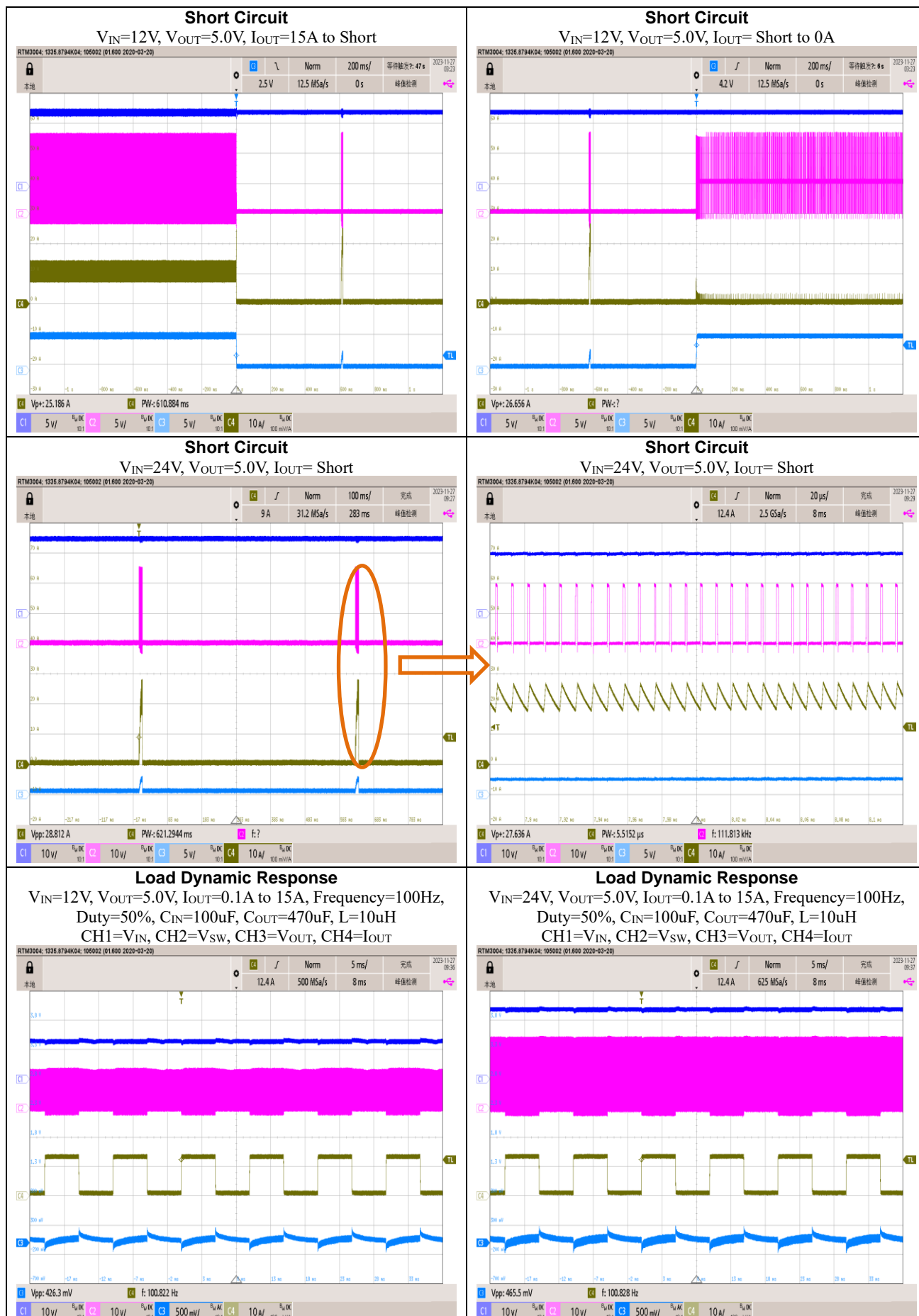
Typical Performance Characteristics

$T_J = 25^\circ\text{C}$, $V_{IN} = 12\text{V}$, unless otherwise noted.



CH1=V_{IN}, CH2=V_{SW}, CH3=V_{OUT}, CH4=I_{SW}, unless otherwise noted.





Operational Description

The NDP1415RB is a high efficiency, monolithic, synchronous step-down DC/DC converter utilizing a Jitter frequency, average current mode control architecture. Average current mode control enables fast and precise control of the output current. It operates through a wide VIN range and regulates with low quiescent current. An error amplifier compares the output voltage with an internal reference voltage of 1.0V and adjusts the peak inductor current accordingly. overvoltage and undervoltage comparators will turn off the regulator.

Main Control Loop

During normal operation, the internal top power switch (N-channel MOSFET) is turned on at the beginning of each clock cycle, causing the inductor current to increase. The sensed inductor current is then delivered to the average current amplifier, whose output is compared with a saw-tooth ramp. When the voltage exceeds the v_{duty} voltage, the PWM comparator trips and turns off the top power MOSFET. After the top power MOSFET turns off, the synchronous power switch (N-channel MOSFET) turns on, causing the inductor current to decrease. The bottom switch stays on until the beginning of the next clock cycle unless the reverse current limit is reached and the reverse current comparator trips. In closed-loop operation, the average current amplifier creates an average current loop that forces the average sensed current signal to be equal to the internal ITH voltage. Note that the DC gain and compensation of this average current loop is automatically adjusted to maintain an optimum current-loop response. The error amplifier adjusts the ITH voltage by comparing the divided-down output voltage (VFB) with a 1.0V

reference voltage. If the load current changes, the error amplifier adjusts the average inductor current as needed to keep the output voltage in regulation.

Low Current Operation

The discontinuous-conduction modes (DCMs) are available to control the operation of the NDP1415RB at low currents. Burst Mode operation automatically switch from continuous operation to the Burst Mode operation when the load current is low.

VIN Overvoltage Protections

To protect the internal power MOSFET devices against transient voltage spikes, the NDP1415RB constantly monitors the VIN pin for an overvoltage condition. When VIN rises above 38V, the regulator suspends operation by shutting off both power MOSFETs. Once VIN drops below 37V, the regulator immediately resumes normal operation. The regulator executes its soft-start function when exiting an overvoltage condition.

Cable Drop Compensation

Due to the resistive of charger's output Cable, The NDP1415RB built in a simple user programmable cable voltage drop compensation using the impedance at the FB pin. Choose the proper resistance values for charger's output cable as show in table 1(According to $CSP-CSN_X=60mV$):

Rup is the upper resistor the resistors divider net.

Rlow is the lower resistor the resistors divider net.

| R _{FB_TOP} (K) | R _{FB_LOW} (K) | Cable Drop compensation (mV) |
|-------------------------|-------------------------|------------------------------|
| 100 | 25 | 75 |
| 160 | 39 | 250 |
| 360 | 91 | 570 |
| 470 | 120 | 750 |
| 820 | 200 | 1400 |
| 1200 | 300 | 2000 |

table 1

Frequency Selection and Shutdown

The switching frequency of the NDP1415RB can be programmed through an external resistor between 130kHz and 300 kHz, Floating this pin set the switching frequency to 130K, an external resistor can set the frequency up to 300KHz. The switching frequency is set using the FS pins as shown in Table 2:

| FS Resistor(K Ω) | Frequency (Hz) |
|--------------------------|----------------|
| Floating | 130K |
| 1000 | 140K |
| 750 | 160K |
| 510 | 170K |
| 300 | 210K |
| 200 | 255K |
| 150 | 300K |

table 2

When the FS pin is below 0.6V, the NDP1415RB enters a low current shutdown state, reducing the DC supply current to 1.3mA.

MOSFET Selection

The maximum inductor peak current is limited by the high-side MOSFET RDSON. the internal current limiting voltage is set to typica 200mV. The larger high-side MOSFET RDSON, the smaller the maximum peak current, and vice versa. The calculation is as follows.

$$I_{PEAKMAX} = V_{IPK} / R_{DS(on)}$$

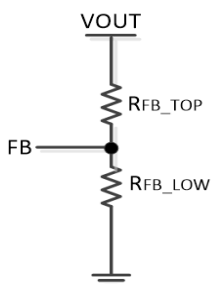
V_{IPK} is the internal current limit reference voltage.

$R_{DS(on)}$ is the high-side MOSFET RON

Constant Voltage Output

NDP1415RB presets the VFB voltage to 1V. The Output can be set by extra resistance.

$$V_{OUT} = V_{FB} * \frac{R_{FB_TOP} + R_{FB_LOW}}{R_{FB_LOW}}$$



Applications Information

Input Capacitor (CIN) Selection

The input capacitance CIN is needed to filter the square wave current at the drain of the top power MOSFET. To prevent large voltage transients from occurring, a low ESR input capacitor sized for the maximum RMS current should be used. The maximum RMS current is given by:

$$I_{RMS} \cong I_{OUT(MAX)} \frac{V_{OUT}}{V_{IN}} \sqrt{\frac{V_{IN}}{V_{OUT}} - 1}$$

This formula has a maximum at $V_{IN} = 2V_{OUT}$, where: $I_{RMS} \cong I_{OUT}/2$

This simple worst-case condition is commonly used for design because even significant deviations do not offer much relief. Note that ripple current ratings from capacitor manufacturers are often based on only 2000 hours of life which makes it advisable to further derate the capacitor, or choose a capacitor rated at a higher temperature than required. Several capacitors may also be paralleled to meet size or height requirements in the design. For low input voltage applications, sufficient bulk input capacitance is needed to minimize transient effects during output load changes.

Output Capacitor (COUT) Selection

The selection of COUT is determined by the effective series resistance (ESR) that is required to minimize voltage ripple and load step transients as well as the amount of bulk capacitance that is necessary to ensure that the control loop is stable. Loop stability can be checked by viewing the load transient response. The output ripple, ΔV_{OUT} , is determined by:

$$\Delta V_{OUT} < \Delta I_L \left(\frac{1}{8 \cdot f \cdot C_{OUT}} + ESR \right)$$

The output ripple is highest at maximum input voltage since ΔI_L increases with input voltage. Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling

requirements. Dry tantalum, special polymer, aluminum electrolytic, and ceramic capacitors are all available in surface mount packages. Special polymer capacitors are very low ESR but have lower capacitance density than other types. Tantalum capacitors have the highest capacitance density, but it is important to only use types that have been surge tested for use in switching power supplies. Aluminum electrolytic capacitors have significantly higher ESR but can be used in cost-sensitive applications provided that consideration is given to ripple current ratings and long-term reliability. Ceramic capacitors have excellent low ESR characteristics and small footprints.

Inductor Selection

Given the desired input and output voltages, the inductor value and operating frequency determine the ripple current:

$$\Delta I_L = \frac{V_{OUT}}{F * L} \left(1 - \frac{V_{OUT}}{V_{IN(MAX)}} \right)$$

Lower ripple current reduces power losses in the inductor, ESR losses in the output capacitors and output voltage ripple. Highest efficiency operation is obtained at low frequency with small ripple current. However, achieving this requires a large inductor. There is a trade-off between component size, efficiency, and operating frequency. A reasonable starting point is to choose a ripple current that is about 40% of $I_{OUT(MAX)}$. To guarantee that ripple current does not exceed a specified maximum, the inductance should be chosen according to:

$$L = \frac{V_{OUT}}{F * \Delta I_{L(MAX)}} \left(1 - \frac{V_{OUT}}{V_{IN(MAX)}} \right)$$

Once the value for L is known, the type of inductor must be selected. Actual core loss is independent of core size for a fixed inductor value but is very dependent on the inductance selected. As the inductance or frequency increases, core losses decrease. Unfortunately, increased inductance requires more turns of wire and therefore copper

losses will increase. Copper losses also increase as frequency increases. Ferrite designs have very low core losses and are preferred at high switching frequencies, so design goals can concentrate on copper loss and preventing saturation. Ferrite core material saturates “hard”, which means that inductance collapses abruptly when the peak design current is exceeded. This results in an abrupt increase in inductor ripple current and consequent output voltage ripple. Do not allow the core to saturate!

Different core materials and shapes will change the size/current and price/current relationship of an inductor. Toroid or shielded pot cores in ferrite or permalloy materials are small and don't radiate much energy, but generally cost more than powdered iron core inductors with similar characteristics. The choice of which style inductor to use mainly depends on the price versus size requirements and any radiated field/EMI requirements. New designs for surface mount inductors are available from Coilcraft, Toko, Vishay, NEC/Tokin, TDK and Würth Elektronik.

Efficiency Considerations

The percent efficiency of a switching regulator is equal to the output power divided by the input power times 100%. It is often useful to analyze individual losses to determine what is limiting the efficiency and which change would produce the most improvement. Percent efficiency can be expressed as: % Efficiency = 100% – (Loss1 + Loss2 + ...) where Loss1, Loss2, etc. are the individual losses as a percentage of input power. Although all dissipative elements in the circuit produce losses, three main sources usually account for most of the losses in NDP1415RB circuits: 1) I^2R losses, 2) switching and biasing losses, 3) other losses.

Thermal Conditions

In most applications, the NDP1415RB does not dissipate much heat due to its high efficiency and low thermal resistance. However, in applications where the NDP1415RB is running at high ambient

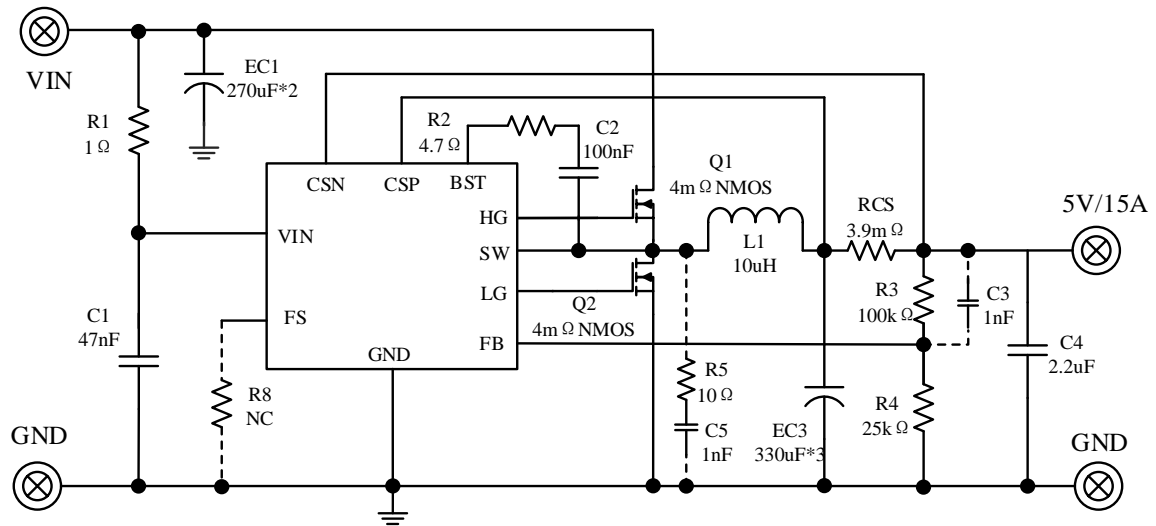
temperature, high VIN, and maximum output current load, the heat dissipated may exceed the maximum junction temperature of the part. If the junction temperature reaches approximately 165°C, both power switches will be turned off until the temperature drops about 30°C cooler to avoid the NDP1415RB from exceeding the maximum junction temperature, the user will need to do some thermal analysis. The goal of the thermal analysis is to determine whether the power dissipated exceeds the maximum junction temperature of the part. If the application calls for a higher ambient temperature

and/or higher switching frequency, care should be taken to reduce the temperature rise of the part by using a heat sink or forced air flow.

EMI/EMC

To solve EMI electromagnetic interference, SW pin should add a circuit of RC filter, a 20Ω resistor and a 1nF capacitor, BST pin reserved 0Ω~5Ω string 100nF. If the application version enough volume, can be reserved at input end type II circuit.

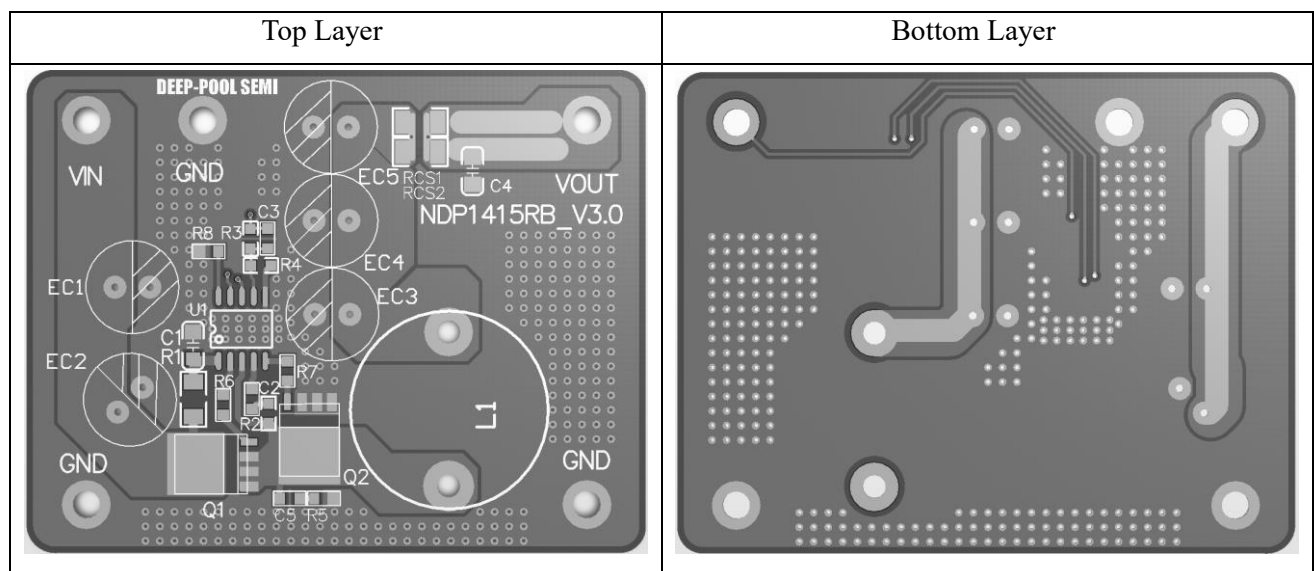
Typical Applications



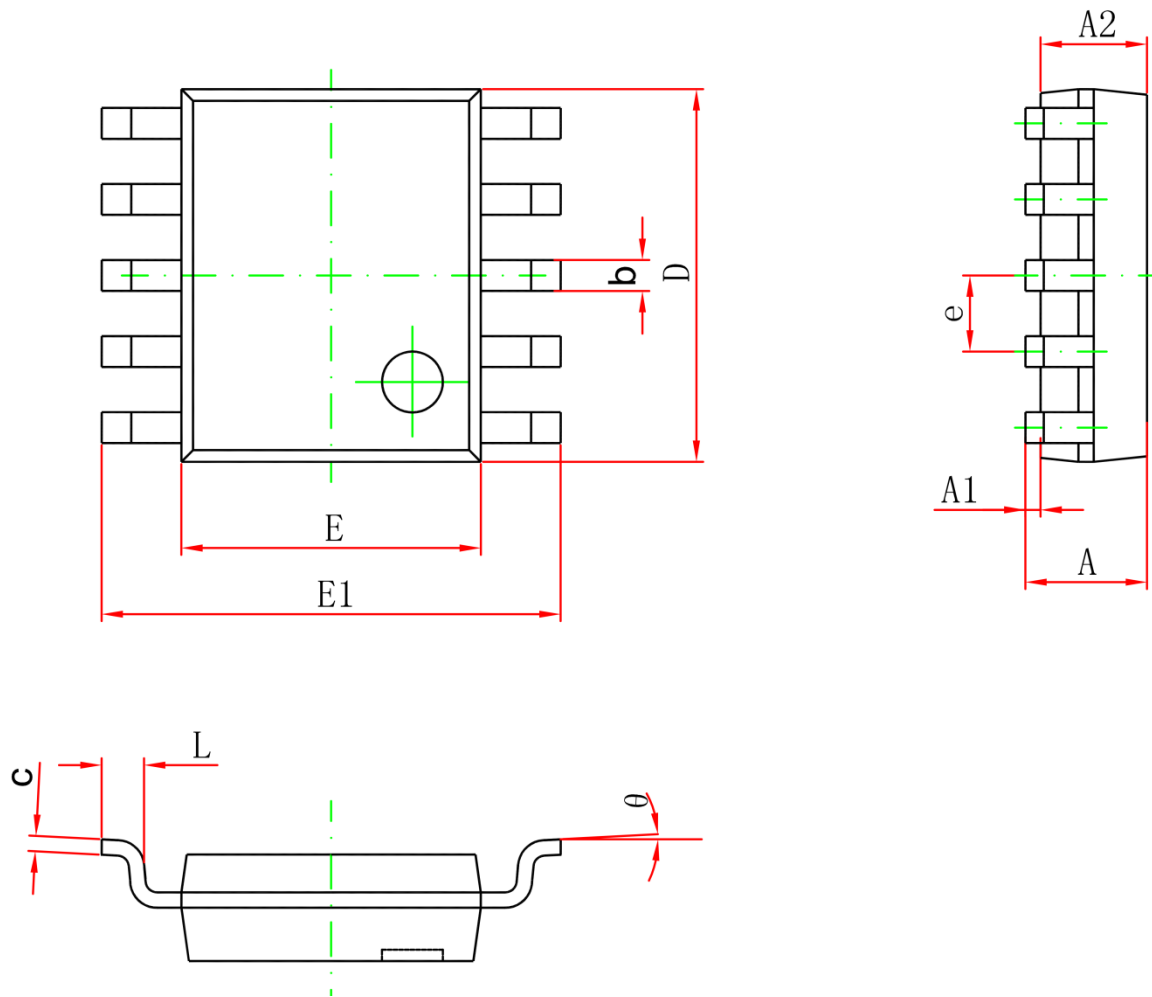
Layout Guide

PCB layout is important to achieve stable operation. For best results, use the following guidelines and figures as reference.

- 1) The electrolytic capacitors EC2 are close to the Drain of Q1.
- 2) The RC filtering(R1&C1) of VIN pin as close to the chip.
- 3) Use short and direct feedback connections, R3 and R4 resistors as shown in the following figure.
- 4) The bootstrap capacitor C2 is placed near the chip pin.
- 5) The input electrolytic capacitor ground, output electrolytic capacitor ground, and MOSFET ground should be placed as close as possible.



Package Outline Drawing



| Dimensional In Millimeters | | | Dimensional In Inches | |
|----------------------------|-------------|-------|-----------------------|-------|
| Ref | MIN | MAX | MIN | MAX |
| A | 1.35 | 1.75 | 0.053 | 0.069 |
| A1 | 0.100 | 0.250 | 0.004 | 0.010 |
| A2 | 1.350 | 1.550 | 0.053 | 0.061 |
| b | 0.300 | 0.450 | 0.012 | 0.018 |
| c | 0.170 | 0.250 | 0.007 | 0.010 |
| D | 4.700 | 5.100 | 0.185 | 0.201 |
| E | 3.800 | 4.000 | 0.15 | 0.157 |
| E1 | 5.800 | 6.200 | 0.228 | 0.244 |
| e | 1.000 (BSC) | | 0.039 (BSC) | |
| L | 0.400 | 1.270 | 0.016 | 0.050 |
| θ | 0° | 8° | 0° | 8° |

Notes

1. Use millimeters as the primary measurement
2. Dimensioning and tolerances conform to ASME Y14.5M. – 1994
3. These dimensions do not include mold flash or protrusions.
4. Mold flash or protrusions shall not exceed 0.15mm

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